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# STRUCTURE AND MAGNETIC PROPERTIES OF THE NIFE FILMS ELECTRODEPOSITED IN NON-STATIONARY MODES

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Abstract. Ni-rich permalloy (NiFe) films were prepared using electrodeposition in different modes from sulfate electrolyte. As modes were determined regime of direct current (DC), pulse current (PC) and pulse-reverse current (RC). Correlation between technological modes of preparation, chemical composition, structural characteristics and magnetic parameters was established. Based on EDX data it was shown that Fe content in samples varied from 17.4 to 42.1 at.%, depending on deposition modes. It opens broad perspectives for chemical control of the permalloy films from one electrolyte. This is technologically convenient. Based on XRD data it was concluded that samples were single-phase. The surface morphology was analyzed using AFM. Pulse-reverse (RC) film surface are rough and have observable mostly fused grains, which significantly differs from DC and PC film surfaces, which are smooth and have no distinguishable grains. The  $R_q$  values of RC film is around 27.9 nm, while DC and PC films have  $R_q$  values of 9.6 nm and 4.1 nm, respectively. Based on DSC data all the phase transitions in investigates samples and their transition temperatures were detected and compared with bulk analogs. Temperature dependences of the magnetic susceptibility and field dependences of the specific magnetization were measured. Main magnetic parameters were established. It was demonstrated that the synthesized NiFe films have a significant magnetic anisotropy. It was demonstrated the correlation between NiFe electrodeposition modes and their magnetic properties. Obtained results open broad perspectives for modification of the standard electrodeposition processes of Ni-rich permalloy films preparation for practical applications in the field of magnetic sensors and shields for electromagnetic protection.

Keywords: NiFe films, electrodeposition, pulse-reverse regimes, magnetic properties.

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## 1 Introduction

The electrodeposition (or electroplating) technique is a widely used for preparation of the alloy films and coatings. Electrodeposited alloy coatings are commonly used as decorative layers

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(Oriňáková et al., 2006; Giurlani et al., 2018); physical, chemical, or electromagnetic protection of devices (Maniam & Paul, 2021; Lelevic & Walsh, 2019; Lisenkov et al., 2010; Papailiou et al., 2010); and electrodeposited alloy films have many applications in microelectronics (Zangari, 2015; Suzdaltsev, 2022; Deligianni, 2006). Moreover, electrodeposition is used in the synthesis of nanostructures (nanorods, nanopillars, nanolayers, and so on) nowadays Stine (2019); Inguanta et al. (2008); Sobha (2012); Nasirpouri (2017). Electrodeposition has many parameters (current density and voltage, pulse and pulse-reverse modes, electrolyte temperature, pH, and stirring) that are capable of influencing on the alloy deposits composition, crystal structure, and microstructure. In addition to composition control in mono, binary, ternary, and more complex alloys, electrodepositions provide the ability to obtain alloys with composition gradients Zubar et al. (2022); Rotkovich et al. (2023); Zubar et al. (2019) or even multilayer structures (Zubar et al., 2020; Vinnik et al., 2021; Warcholinski et al., 2017).

Electrodeposited NiFe alloys are of great importance in a wide range of applications. Ni-rich alloys (Ni<sub>80</sub>Fe<sub>20</sub> "permalloy" and alloys with close composition) are magnetically soft materials with low coercivity and extremely high magnetic permeability (Vahdatid et al., 2018; Zhang et al., 2012; English et al., 1967; Rizal & Niraula, 2015). They are mostly known for their anisotropic and giant (in multilayer films) magnetoresistance and are used in magnetoresistive devices in hard disks (Lee et al., 2000; Vieux-Rochaz et al., 2000; Pasa & Schwarzacher, 1999). Moreover, they have such applications as electromagnetic shielding (Park et al., 2019; Kanafyev et al., 2022; Graf & Vance, 1988), magnetic field sensors (Seet et al., 2007; Hika et al., 1996), magnetic proximity effect and spin Hall effect (Mazraati et al., 2016; Ma et al., 2020; Zhu et al., 2018), and magnetoresistive random-access memory (MRAM) (?Almeida et al., 2022).

Modification of the synthesis conditions of the electrodeposited NiFe alloy structures makes it possible to obtain the widest range of their chemical composition, crystal structure and grain structure (Llavona et al., 2013). Electrodeposition bath composition, pH, bath temperature and agitation conditions, current parameters and modes, deposition in the magnetic field or ultrasonic radiation are the most common levers used to modify NiFe alloy deposits characteristics (Zubar et al., 2019; Horkans, 1981; Fedkin et al., 2023). Thus, pulsed electrodeposition allows to change NiFe alloys features significantly as compared to the alloys electrodeposited in direct current (Zubar et al., 2021; Salem et al., 2012; Grimmett et al., 1993). Pulse current duration and pause combination expand Fe content range (upside mostly) and decrease crystallites and grain sizes in particular (Kockar et al., 2004; Torabinejad et al., 2017; Blythe et al., 1996).

Pulse-reverse electrodeposition mode (RC) is of no less importance. There are reverse (anodic) current pulses in the duty cycle, which make it different from the pulse mode and cause short-term deposit dissolution. Wherein cathodic current pulses alternate with anodic current pulses, as well as with pauses (or without pauses in many works). Pulse-reverse electrodeposition has a complex influence on composition and microstructure of the NiFe alloys (Schultz & Pritzker, 1998; Flynn & Desmulliez, 2010). In the experiments with electrolyte baths similar to ours (sulfate baths with similar additives), a decrease in the Fe content and increased grains vertical growth were described (Wasekar et al., 2016; Williams et al., 1996; Fedosyuk et al., 1991). In our previous work Kotelnikova et al. (2022), we gave a detailed explanation of the mechanism that corresponded to the change in the films composition and grains vertical growth intensity when changing DC and PC modes to RC mode.

In the present work, we analyzed correlation between different modes of electrodeposition (direct current - DC, pulse current - PC and pulse-reverse current - RC) on structural characteristics and magnetic properties of the Ni-rich permalloy films.

# 2 Experimental

The electrodeposition or electrolyte deposition method was used to obtain alloy NiFe films. The polished steel plates were used as substrates for electrodeposition. The plate width and length

were 400 mm, and one side of the plate was isolated by dielectric to deposit film on another side only. The polished steel substrates were chosen for easy films separation from them and following investigations.

The NiFe films were deposited in the complex sulfate electrolyte. The composition of electrolyte presented it Table 1.

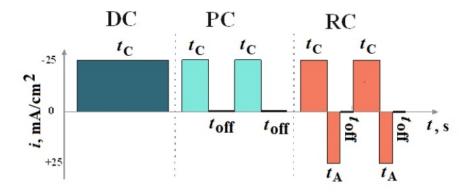
Table 1:	Chemical	composition of	of electrolyte for	preparation of	the electrodeposited NiFe films.
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Chemical component	Concentration, g/L				
Main components					
1. $FeSO_4 \cdot 7H_2O$	15				
2. $NiSO_4 \cdot 7H_2O$	210				
3. NiCl <sub>2</sub> ·6H <sub>2</sub> O	20				
Additional components					
1. H <sub>3</sub> BO <sub>3</sub>	30				
$2. \text{ MgSO}_4 \cdot 7\text{H}_2\text{O}$	60				
3. $KNaC_4H_4O_6\cdot 4H_2O$	30				
Additives					
1. C <sub>6</sub> H <sub>7</sub> O <sub>6</sub> (citric acid)	2				
2. C <sub>7</sub> H <sub>5</sub> NO <sub>3</sub> S (saccharin)	2				

The electrolyte temperature was kept at  $35^{\circ}$ C, and the pH was kept at 2.4. The current density was  $25 \text{ mA/cm}^2$  for direct and reverse currents. The electrodeposition current parameters are presented in Table 2.

**Table 2:** The electrodeposition current parameters for NiFe films preparation in direct current mode (DC), pulse mode (PC) and pulse-reverse (RC) modes.

Sample	Duration	Duration	Duration	Total depo-	Effective de-
acronym	of ca-	of pause	of anodic	sition time,	position time,
	thodic	$(t_{off}),\mathrm{ms}$	(reverse)	min	min
	current		current		
	$(t_C),$		$(t_A),  \mathrm{ms}$		
	ms				
DC	$3.6 \cdot 10^6$	-	-	60	60
PC	100	100	-	120	60
RC	100	75	25	160	60



**Figure 1:** A schematic representation of direct (DC), pulsed (PC) and pulse-reverse (RC) current modes for NiFe films electrodeposition.

The DC sample was obtained in direct current mode for 60 min. The PC sample was

deposited in pulse current mode with a cathodic current pulse  $t_C$  of 100 ms and an equal pause duration  $t_{off}$  for 120 min in total. RC sample was obtained in pulse-reverse current mode with a cathodic current pulse of 100 ms. The anodic (reverse) current pulse  $t_A$  was 25 ms and pause was 75 ms. The electrodeposition mode scheme is presented in Figure 1.

The total deposition time and effective deposition time parameters were used to deposit NiFe film with close thicknesses. The total and effective deposition times were equal for the DC sample, as the cathodic current was applied to it continuously. The total deposition time for pulse and pulse-reverse modes was calculated using:

$$t_{TD} = t_{ED} \times \frac{t_C + t_A + t_{OFF}}{t_C - t_A},$$
 (1)

where  $t_{TD}$  is total deposition time, ms;  $t_{ED}$  is effective deposition time, ms;  $t_C$  is cathodic current pulse duration, ms;  $t_{OFF}$  is pause duration, ms; and  $t_A$  is anodic (reverse) current pulse duration, ms.

The chemical composition was investigated by energy-dispersive X-ray spectroscopy on AZtecLive Advanced with Ultim Max 40 (Oxford Instruments, Bognor Regis, UK). The precision of the measurements  $\sigma$  was  $\pm$  0.1 at. %. The crystal structure was studied by XRD on the powder diffractometer EMPYREAN (PANalytical, Malvern Instruments, Malvern, UK) using Cu- $K\alpha$  radiation in the Bragg–Brentano geometry focusing in the angle range  $2\theta = 40$  – 100°. The coherent scattering regions sizes were estimated using the Williamson–Hall method for all peaks in the fcc solid solution. The precision of the measurements  $\sigma$  was  $\pm$  0.01 % for peak intensity,  $\pm$  1· $10^{-4}$  nm for unit cell parameter, and  $\pm$  1 nm for coherent scattering region.

The surface microstructure was investigated using the atomic force microscope (AFM) NT-206 (Microtestmachines, Gomel, Belarus). The contact scanning mode was used to obtain AFM images. A silicon tip with a curvature radius of 10 nm and a force constant of 0.6 N/m was used during AFM scanning. Grain sizes were measured using AFM images ( $20\times20~\mu\mathrm{m}$ ) of free films via the Gwyddion software. To recognize the grains, the method of marking grains by the watershed was used.

Thermal analysis was carried out using a differential scanning calorimeter (DSC) 404 F3 Pegasus (NETZSCH, Germany) at a temperature range of  $30-1500^{\circ}\mathrm{C}$  in the gaseous atmosphere – argon (Ar). The measurement was carried out at a constant heating rate 10 K/min. The measurement results were processed using the Proteus software supplied with the measuring equipment.

The magnetic parameters were investigated at a temperature range of  $4.2-900~\mathrm{K}$  using the Liquid Helium Free High Field Measurement System (Vibrating Sample Magnetometer – VSM) (Cryogenic Limited, London, UK). The applied magnetic field was from -3 to +3 T, and the precision of the measurements for specific magnetization  $\sigma$  was  $\pm$  0.01  $\mathrm{A \cdot m^2 \cdot kg^{-1}}$ .

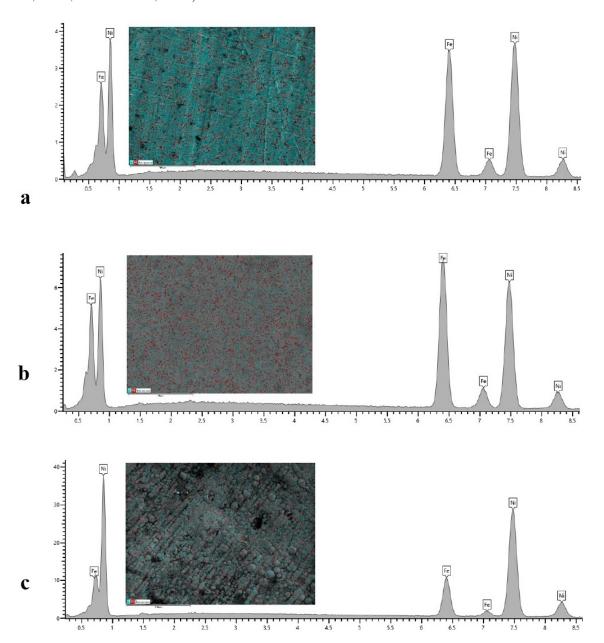
# 3 Results and discussion

#### 3.1 Structural characteristics

The energy-dispersive X-ray spectroscopy (EDX) was used to investigate the chemical composition of the NiFe films. Figure 2 demonstrates EDX-spectra and elemental mapping for prepared samples. There is an increase in the Fe concentration when changing from DC (36.4 at.%) to pulse current mode (42.1 at.%). The Fe content is increased due to the intensification of the Fe ions diffusion during the pauses.

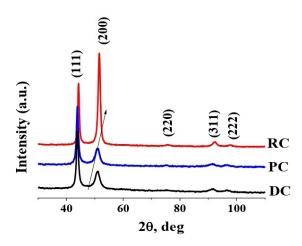
There is a sharp decrease (from 42.1 to 17.4 at. %) in the Fe content during the transition from pulse (PC sample) to pulse-reverse (RC sample) electrodeposition mode. It is due to the higher Fe than Ni oxidation (and dissolution) rate during anodic pulses as well as Fe hydroxides transfer from the near-sample area into the bulk of the electrolyte during both anodic pulses and pauses, which weakens the anomalous character of the NiFe codeposition. A more detailed

description of chemical composition correlations is presented in our previous works (Kotelnikova et al., 2022; Zubar et al., 2021).



**Figure 2:** EDX-spectra and elemental mapping (on insert) of the NiFe films prepared in direct current modes: (a) DC; (b) PC and (c) RC.

The X-ray diffraction structural analysis (XRD) patterns are presented in Figure 3. All the peaks correspond to face-centered cubic lattice atomic planes, and no peaks correspond to body-centered atomic planes. It indicates that a Fe solid solution in Ni was formed in all the films samples. Crystal structure parameters obtained from XRD are presented in Table 3.



**Figure 3:** XRD patterns of the NiFe films prepared in direct current modes (DC), pulse mode (PC) and pulse-reverse (RC) modes.

**Table 3:** Crystal structure parameters of the NiFe films obtained in different electrodeposition modes.

Sample	a, nm	V, nm <sup>3</sup>	$I_{200}/I_{111},$	CSR,
acronym			%	nm
DC	0.3570	0.0455	73	~6
PC	0.3571	0.0455	63	~7
RC	0.3572	0.0456	211	~10

The DC and PC samples have very close coherent scattering regions (CSR) sizes and unit cell parameters of  $^{\sim}6-7$  nm. The sample RC has a CSR size of  $^{\sim}10$  nm. There is also a significant increase in the peaks integral intensities ratio  $I_{(200)}/I_{(111)}$  with transition from pulse to pulse-reverse mode. It means that film crystals grew in a predominant direction (200) during the pulse-reverse mode.

Figure 4 presents atomic force microscopy (AFM) images of the NiFe films surface. Gwyddion software was used to investigate grain sizes in AFM images. It was impossible to distinguish the grains of the DC and PC films to evaluate their sizes. The DC and PC samples have a smooth surface without distinguishable grains. While DC film has a lot of pores and PC film is almost poreless. Pulse-reversed film surfaces significantly differ from DC and PC films and have observable, mostly fused grains. The reason for such a difference in microstructure is the features of saccharine's (brightening additive in the electrolyte) behavior in direct, pulse, and pulse-reverse electrodeposition modes, which were discussed previously (Kotelnikova et al., 2022).

Root mean square (RMS) surface roughness was determined via Gwyddion software from AFM images of the films. DC film has an Rq of 9.6 nm, and PC film has an Rq of 4.1 nm. Surface roughness decreases with the transition from direct to pulse current, which is related to the higher nucleation rate in pulse mode. RC film has Rq value of 27.9 nm. RC film has higher surface roughness than DC and PC films, which is related to promoted grains vertical growth in pulse-reverse mode.

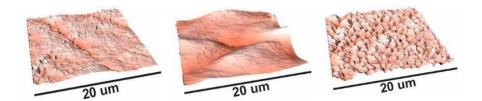


Figure 4: Surface morphology of NiFe films investigated using AFM: (a) DC; (b) PC and (c) RC.

#### 3.2 Phase transitions

Figure 5 demonstrates the results of the differential scanning calorimetry (DSC) investigations of the NiFe films obtained in the different electrodeposition modes. DSC curves include both nonmagnetic second-order phase transition peaks and magnetic second-order phase transition peaks.

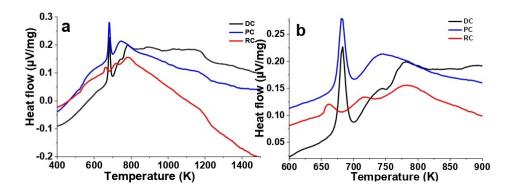


Figure 5: DSC curves of the NiFe films obtained in different electrodeposition modes: in the temperature range 400-1500 K (a) and enlarged DSC curves in the range 600 - 900 K (b).

Nonmagnetic and magnetic phase transition temperatures for bulk NiFe alloys in accordance [53] with compositions similar to NiFe films by us are shown in Table 4.

The temperatures of the nonmagnetic phase transitions (from DSC curves) and proposed phase transitions of the NiFe alloy film are presented in Table 5. It was found that DC film has only two nonmagnetic phase transitions (682 and 744 K) instead of three transitions in the bulk alloy of the same chemical composition (604, 645, and 739 K). The PC sample has only one phase transition instead of two (619 and 787 K). RC film has the same number of phase transitions and very close transition temperatures as the bulk alloy (film – 660 and 718 K, bulk alloy – 678 and 719 K).

Table 4: Phase transitions temperatures of the NiFe bulk alloys (Vernyhora et al., 2012).

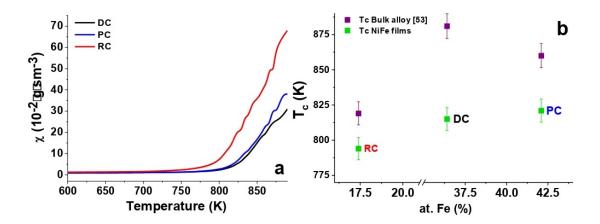
Type of phase transition in	Fe concentration, at.%		
Ni-Fe system			
	~36.4	~42.1	~17.4
$T_{ph}(\alpha - Fe - Ni + FeNi_3 \leftrightarrow FeNi_3)$	604 K	-	-
$T_{ph}(FeNi_3 \leftrightarrow \gamma - Fe - Ni + FeNi_3)$	645 K	-	678 K
$T_{ph}(\gamma - Fe - Ni + FeNi_3 \leftrightarrow \gamma - Fe - Ni)$	739 K	787 K	719 K
$T_{ph}(\alpha - Fe - Ni + FeNi_3 \leftrightarrow \gamma - FeNi + FeNi_3)$	-	619 K	-
$T_{\rm ph}(FeNi_3 \leftrightarrow \gamma - Fe - Ni)$	-	-	-
$T_{\rm ph}(\gamma - Fe - Ni(FM) \leftrightarrow \gamma - Fe - Ni(PM))$	881 K	860 K	819 K

Type of phase transition in Ni-Fe system	Fe concentration, at.%		
	~36.4	~42.1	~17.4
	DC	PC	RC
$T_{\rm ph}(a-Fe+FeNi_3\leftrightarrow g-Fe-Ni)$	-	682 K	-
$T_{\rm ph}(a-Fe+FeNi_3\leftrightarrow g-Fe-Ni+FeNi_3)$	682 K	-	-
$T_{\rm ph}(g-Fe-Ni+FeNi_3\leftrightarrow g-Fe-Ni)$	744 K	-	718 K
$T_{\rm ph}(FeNi_3 \leftrightarrow g - Fe - Ni)$	-	-	-
$T_{\rm ph}FeNi_3 \leftrightarrow g - Fe - Ni + FeNi_3)$	-	-	660 K

Table 5: Phase transitions temperatures of the NiFe alloy films obtained from DSC curves.

## 3.3 Magnetic properties

Figure 6 demonstrates temperature dependences of the magnetic susceptibility (fig. 6a) and concentration dependences of the magnetic phase transition (Curie temperature or  $T_c$ ) – fig. 6b determined by Faraday technique.



**Figure 6:** Temperature dependences of the magnetic susceptibility (a) and concentration dependences of the magnetic phase transition (b) determined by Faraday technique.

Results of the NiFe alloy films Curie temperature measurement by Faraday technique are presented also in Table 6. The magnetic transition temperature  $T_c$  (Faraday) for DC and PC samples is 815 and 821 K, respectively. RC films has  $T_c$   $\tilde{}$  794 K.

It was found that all the electrodeposited films have lower Curie temperatures as compared with those in the NiFe phase diagram for bulk NiFe alloys of the same compositions Zubar et al. (2021). That decrease is caused by the transition from bulk to 2D-objects. The Tc values for DC-PC-RC samples correlate well with average Fe content in electrodeposited films.

Figure 7 demonstrates field dependences of the specific magnetization for DC-PC-RC NiFe films. Field dependences of M(B) dependences were measured by VSM in the wide range of magnetic fields (up to 3 T) for perpendicular and parallel orientation to the film surface.

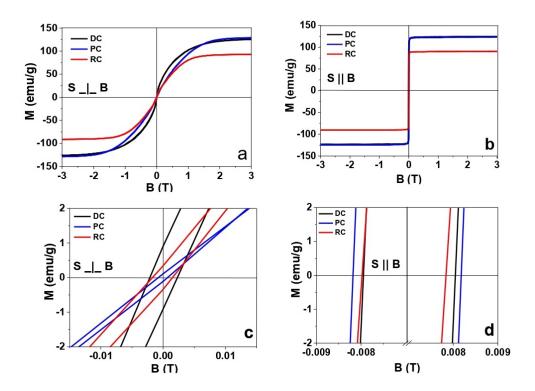


Figure 7: Field dependences of the specific magnetization of the NiFe films obtained in different electrodeposition modes: (a) magnetic field (in the range up to 3 T) oriented perpendicular to the film plane, (b) magnetic field (in the range up to 3 T) oriented parallel to the film plane, (c) enlarged for perpendicular orientation and (d) enlarged for parallel orientation.

**Table 6:** Main magnetic parameters of the NiFe films obtained in different electrodeposition modes in perpendicular and parallel field orientations: magnetization saturation  $(M_s)$ ; remnant magnetization  $(M_r)$ ; coercivity  $(H_c)$ ; saturation field  $(H_s)$  and squareness coefficient (SQR).

Magnetic parameters	Sample acronym		
	DC	PC	RC
	S_ _B		
$M_s$ , emu/g	114.4	121.7	89.8
$M_r$ , emu/g	0.9	0.1	0.4
$H_c$ , Oe	21.5	7.7	17.5
$H_s$ , kOe	19.6	21.7	18.1
$SQR (M_r/M_s), \cdot 10^{-4}$	79	9	38
	S   B		
$M_s$ , emu/g	121.8	132.6	89.4
$M_r$ , emu/g	108.2	113.1	81.1
$H_c$ , Oe	83.7	87.6	81.9
$H_s$ , kOe	1.4	1.0	1.5
$SQR (M_r/M_s), \cdot 10^{-4}$	8911	8502	9134

The significant magnetic anisotropy of the NiFe films magnetic parameters defined from the M(B) dependences is presented in Table 6. According to the out-of-plane measurements (perpendicular field orientation), the coercivity ( $H_c$ ) of the sample DC is equal to ~21.5 Oe, whereas the PC film's coercivity is ~7.7 Oe. There is a  $H_c$ ~17.5 Oe for RC. Saturation field  $H_s$  has the following values: DC – 19.6, PC – 21.7 and RC – 18.8 kOe. Saturation magnetization  $M_s$  is 114.4, 121.7 and 89.8 emu/g. Remnant magnetization  $M_r$  is 0.9, 0.1 and 0.4 emu/g for DC, PC and RC films, respectively. Hysteresis loop squareness  $M_r/M_s$  is: DC – 0.0079, PC – 0.0009 and RC – 0.0038.

The easy magnetization axis is located in the plane of all the NiFe films. All the samples have similar values of the  $H_c$ during the in-plane (parallel orientation) study: DC - 83.7, PC - 87.3 and RC - 81.9 Oe. Saturation field  $H_s$  has the following values: DC - 1.4, PC - 1.0 and RC - 1.5 kOe. Saturation magnetization  $M_s$  is 121.8, 132.6 and 89.4 emu/g. Remnant magnetization  $M_r$  is 108.2, 113.1 and 81.1 emu/g for DC, PC and RC films, respectively. Hysteresis loop squareness  $M_r/M_s$  is: DC - 0.8911, PC - 0.8502 and RC25 - 0.9134.

# 4 Conclusions

A set of NiFe alloy films was electrodeposited in direct, pulse, and pulse-reverse current modes in a single sulfate bath. The samples Fe content varied from 17.4 to 42.1 at. %, depending on deposition modes. It was demonstrated broad perspectives for chemical control (Fe/Ni ratio) of the electrodeposited Ni-rich permalloy films from one electrolyte. This is technologically convenient. All the samples showed characteristic peaks of fcc lattice atomic planes during XRD investigations. It indicates that all samples are single-phase and Fe solid solution in Ni was formed in all the film samples.

Pulse-reverse (RC) film surface are rough and have observable mostly fused grains, which significantly differs from DC and PC film surfaces, which are smooth and have no distinguishable grains. The  $R_q$  values of RC film is around 27.9 nm, while DC and PC films have  $R_q$  values of 9.6 nm and 4.1 nm, respectively.

According to the DSC investigations, all the electrodeposited films have different numbers of nonmagnetic phase transitions and transition temperatures from their bulk analogs in the NiFe phase diagram in (Vernyhora *et al.*, 2012).

The synthesized NiFe films have a significant magnetic anisotropy. The coercive force  $H_c$  of the NiFe films during the sample in plane investigations is  $\sim 2$ –12 times greater than during sample out of plane investigations. Remnant magnetization  $M_r$  of the NiFe films during the sample in plane investigations is  $\sim 40$ –1000 times greater than during sample out of plane investigations.

Obtained results open broad perspectives for Ni-rich permalloy films preparation with variable Fe content and different microstructure for practical applications in the field of magnetic sensors and shields for electromagnetic protection.

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